

ECON4140 2019 (draft): diff.eq. (systems).

Draft \rightsquigarrow could be revised, especially when it comes to what is exam relevant.

FMEA 6.1–6.3 (Norw.: MA2 2.1–2.3) You must know that if you are given two non-proportional solutions u_1 and u_2 of a *homogeneous linear 2nd order* diff.eq., you obtain the general solution as an arbitrary linear combination $C_1u_1 + C_2u_2$. (FMEA thm 6.2.1, MA2 setning 2.2.1 jf. 2.2.2). In the non-homogeneous case, you need the general solution of the corresponding homogeneous, plus a particular solution u^* of the inhomogeneous.

- Non-constant coefficients: not in itself curriculum: you won't get that equation, and "solve!". But given how to find u_1 , u_2 , u^* , you shall be able to apply the general theory to come up with the answer $C_1u_1 + C_2u_2 + u^*$.
- In particular, this goes for Euler's differential equation (a subsection in FMEA; MA2 avsnitt 2.5). See the seminar problem and the remark given.

Constant coefficients (but variable right-hand side $f(t)$): You shall be able to solve the homogeneous completely, and the types of RHS's given. In particular: if the RHS is t^m , then you might need lower-order terms than m ; and, if the RHS is $e^{\delta t} \sin(qt)$, you need $e^{\delta t} (K \cos(qt) + L \sin(qt))$, etc. Note also what happens if $f(t)$ is a particular solution of the corresponding homogeneous equation.

Constant coeff's only: Stability of linear 2nd order diff.eq's (FMEA section 6.4, MA2 avsnitt 2.6) – and systems in \mathbb{R}^2 (FMEA sections 6.6–6.7, MA2 avsnitt 2.7–2.8). For 2nd order diff.eq's $\ddot{x} + a\dot{x} + bx = 0$:¹

- Globally asymptotically stable $\iff a > 0$ & $b > 0$.
- If $a < 0$ and/or $b < 0$: unstable.
- If $b > 0 = a$: Undamped oscillations $A \cos(t\sqrt{b}) + B \sin(t\sqrt{b})$. Stable, but not asymptotically so (sometimes referred to as «neutrally stable») in the literature.
- If $b = 0 = a$, i.e., the equation $\ddot{x} = 0$: The affine function $C + Dt$, unstable.

Systems $\begin{pmatrix} \dot{x} \\ \dot{y} \end{pmatrix} = \mathbf{A} \begin{pmatrix} x \\ y \end{pmatrix}$ in \mathbb{R}^2 (see however handwritten attachment):

- Reduced to 2nd order diff.eq.'s, with characteristic roots = the eigenvalues of \mathbf{A} , that is: $\lambda_{\pm} = \frac{\text{tr } \mathbf{A}}{2} \pm \sqrt{\left(\frac{\text{tr } \mathbf{A}}{2}\right)^2 - \det \mathbf{A}}$. As with 2nd orders: if these are not real numbers, you put $\alpha = \frac{\text{tr } \mathbf{A}}{2}$ and $\beta = \sqrt{\det \mathbf{A} - \left(\frac{\text{tr } \mathbf{A}}{2}\right)^2}$ and use the formula. (See remark at the end concerning complex numbers.)

¹Norwegian: Enkelte gamle utgaver av MA2 har en trykkfeil om det følgende. 2013-versjonen er riktig.

- In particular, you are expected to tell whether an *unstable* system is a *saddle point*: when the eigenvalues are real and of opposite sign ($\Leftrightarrow \det \mathbf{A} < 0$). For saddle points you shall know that the *convergent* particular solutions have the slope of the eigenvector \mathbf{v} associated to the *negative* eigenvalue. (Slope $y(t)/x(t) = v_2/v_1$ then.)

The “simplest” linear systems $\dot{\vec{x}} = \mathbf{A}\vec{x}$ in \mathbb{R}^n : If \mathbf{A} (assumed constant!) has n *distinct* real eigenvalues $\lambda_1, \dots, \lambda_n$ with eigenvectors $\mathbf{v}^{(1)}, \dots, \mathbf{v}^{(n)}$ then: $C_1\mathbf{v}^{(1)}e^{\lambda_1 t} + \dots + C_n\mathbf{v}^{(n)}e^{\lambda_n t}$. These C_i can be fit to any given initial state; if $\vec{x}(0)$ is given, then $\vec{C} = \mathbf{V}^{-1}\vec{x}(0)$, where \mathbf{V} has the eigenvalues as columns.

(Also true, but not curriculum relevant: replace “real” by “complex”.)

Nonlinear systems. (No global asymptotic stability, so NOT FMEA Theorem 6.8.2.)

- Phase plane analysis: exam ambition is to «sketch» a phase diagram, so that things look qualitatively right: trajectories should be vertical/horizontal across the respective nullclines, up/down and left/right directions should be correct).
- Classification of equilibrium points through eigenvalues of the Jacobian. Note the cases where the test is inconclusive: if the largest eigenvalue is zero, we cannot tell if stable or not; if $\lambda_2 > \lambda_1 = 0$ it is unstable, but we cannot tell whether it is a saddle point.
 - In particular, concerning saddle points: The particular solutions that converge to the saddle point, will *in the limit* converge like the eigenvector \mathbf{v} corresponding to the negative eigenvalue. More precisely: If the saddle point is (x_*, y_*) , then $\lim_{t \rightarrow +\infty} \frac{y(t) - y_*}{x(t) - x_*} = v_2/v_1$ (except slope \rightarrow vertical if $v_1 = 0$).
- *Not* curriculum: Lyapunov functions and Olech’s theorem (part of FMEA sec. 6.8; MA2 avsnitt 2.12). One seminar problem is taken from there, but that problem only asks you for *local* classification, which *is* curriculum.

Complex numbers: you can do without! At the exam you need nothing. In teaching, you will have to deal with the term «real part». The real part of a real number is the number itself, but if the formula for a quadratic yields, e.g., $r = 7 \pm \sqrt{-4}$, then the real part is 7. (Regardless of whether « \pm » is + or –.) Take note that if the quadratic function has no zeroes, then this real part is the stationary point.

Similar goes for a 2×2 matrix \mathbf{A} with characteristic equation $\lambda^2 - \lambda \operatorname{tr} \mathbf{A} + \det \mathbf{A} = 0$: Formula yields $\frac{\operatorname{tr} \mathbf{A}}{2} \pm \sqrt{\left(\frac{\operatorname{tr} \mathbf{A}}{2}\right)^2 - \det \mathbf{A}}$. Real part = λ if real; otherwise, $\frac{\operatorname{tr} \mathbf{A}}{2}$.

"Non-borderline" cases

$$\max_k \operatorname{Re} \lambda_k \neq 0$$

⊛ Generally, \mathbb{R}^n
 $\max_k \operatorname{Re} \lambda_k < 0 \Rightarrow$ $\left\{ \begin{array}{l} \text{local asympt. stability} \\ \text{global if the system} \\ \text{is linear,} \end{array} \right.$

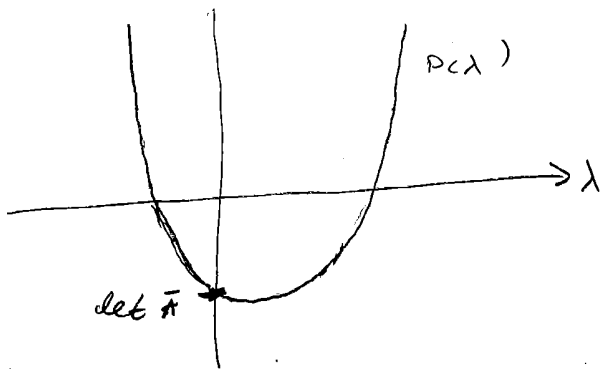
$\max_k \operatorname{Re} \lambda_k > 0 \Rightarrow$ unstable

⊛ \mathbb{R}^2 ,

$$\lambda^2 - \lambda \operatorname{tr} \bar{A} + \det \bar{A} = 0$$

$\underbrace{\hspace{10em}}_{P(\lambda)}$

• Case $\det \bar{A} < 0$: $p(0) < 0$



Opposite-sign real eigenvalues.
(Unstable) saddle point.

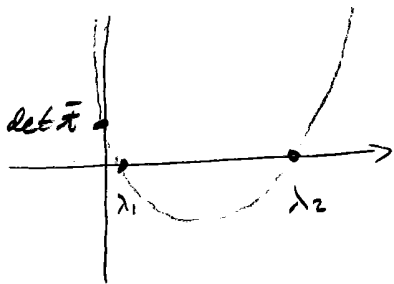
\mathbb{R}^2 cont'd,

Cases with $\det \bar{A} > 0$:

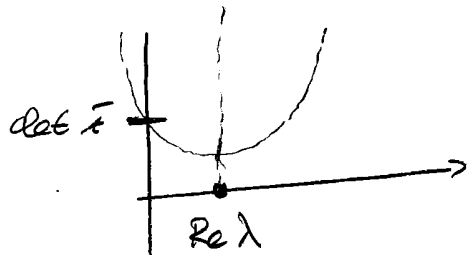
$$p(0) = \det \bar{A} > 0$$

$$p'(0) = -\text{tr} \bar{A}$$

• $\text{tr} \bar{A} > 0$:



or



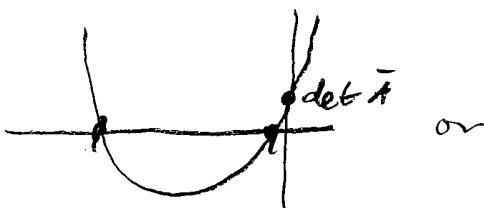
→ Both eigenvalues real & positive. Unstable. ("source")

→ Also valid for the double-eigenvalue case $\lambda_1 = \lambda_2 > 0$

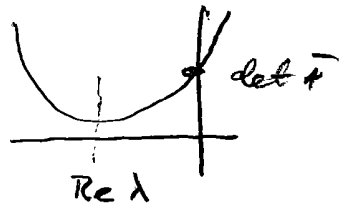


→ No real λ .
 → $\text{Re} \lambda =$ the symmetry axis = the minimum point for $p(\lambda)$
 $= \frac{\text{tr} \bar{A}}{2}$
 → $\text{Re} \lambda > 0$
 ⇒ unstable, outwards spiraling

• $\text{tr} \bar{A} < 0$: Mirror about vertical axis



or

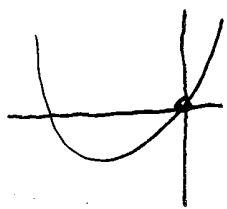


Stable. ("Sink")
 Also valid for $\lambda_1 = \lambda_2 < 0$

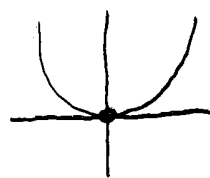
No real λ .
 $\text{Re} \lambda < 0$.
 Stable, spiral inwards

For the following cases, we can classify a linear system $(\dot{x}) = \bar{A}(x)$ completely, but the Jacobian $\bar{A} = J(x^*, y^*)$ of a nonlinear system can at most give partial information

- Case $\text{tr} \bar{A} = \lambda_1 + \lambda_2 < 0, \lambda_1 < \lambda_2 = 0 = \det \bar{A}$
 - Linear system: stable, but not asymptotically
 - Nonlinear: cannot decide stability, but either sink or saddle



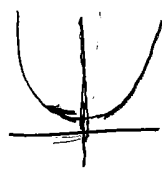
- Cases $\lambda_1 = \lambda_2 = 0 = \det \bar{A} = \text{tr} \bar{A}$



Linear: unstable
("C + Dε")

Nonlinear: could be anything!

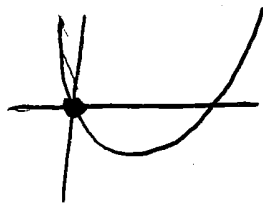
$\det \bar{A} > 0 = \text{tr} \bar{A}$,
 $\text{Re} \lambda = 0$, no real λ



Linear: ellipses
(stable, but not asymptotically)

Nonlinear: cannot decide stability,
but: orbiting spirals or ellipses

- Case $0 = \lambda_1 < \lambda_2 = \text{tr} \bar{A}$
 $0 = \det \bar{A}$ Unstable.



Linear: 

Nonlinear: cannot tell source / saddle